

# Optical Interference Filters Transmission Performance Efficiency Under Temperature Variations Effects

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**Abstract**— This paper has presented optical interference filters transmission performance under thermal temperature effects. Different materials are deeply studied to show the best for optical filtering.

**Index Terms**— Optical filtering, Transmission modulation depth, Optical density, Filter correction and Optical transmission regions.

## I. INTRODUCTION

Optical filters are devices which selectively transmit light of certain properties while blocking (absorbing) the remainder. In general they're sensitive to light of particular wavelengths (and in consequence color) or range of wavelengths. This property makes optical filters often used in many industrial applications. In many branches of industry source emitting intense non-visible radiation (for example white hot metal or glass) has to be monitored. Optical filters are often used for such applications. In such cases infrared (IR) or heat absorbing filters are used in order to block mid infrared wavelengths (thermal radiation) but allow visible light to be transmitted. Additionally, neutral density filters are often used in order to reduce the intensity of light by reflecting or absorbing a portion of it [1, 2]. As a light beam passes through a transparent or translucent material (filter), part of its electromagnetic radiation is absorbed. The amount absorbed electromagnetic radiation depends on [3]: the wavelength; the amount of the absorbing material in the radiation path (filter thickness); the absorption coefficient of the material at that wavelength. Systems with greatly improved optical filters, i.e., filters that provide sub angstrom spectral resolution, rapid wavelength tuning, low wavefront distortion (for imaging), and high throughput, will be needed. The challenge in remote sensing

is to provide rugged, easily used [4], relatively inexpensive devices that can project an image of contaminant concentrations on a screen and record measurements for long-term research. The challenge in optical communications is to integrate extremely inexpensive and rapidly tunable devices into existing systems [5-7].

## II. Filter Model Analysis

The intensity of an incident beam drops exponentially as it passes through the absorber. This is often expressed as the following [5, 8-10]:

$$T_F = P e^{-\alpha_\lambda t} \quad (1)$$

Where  $\alpha_\lambda$  is the filter absorption coefficient at wavelength  $\lambda$ ,  $t$  is the filter thickness, and  $P$  is the filter correction factor which can be defined as the following formula [5, 11- 13]:

$$P = 1 - 2 \left( \frac{n-1}{n+1} \right)^2 + \left( \frac{n-1}{n+1} \right)^4, \quad (2)$$

Therefore filter correction factor percentage is given by the following expression [5]:

$$P(\%) = \left[ 1 - 2 \left( \frac{n-1}{n+1} \right)^2 + \left( \frac{n-1}{n+1} \right)^4 \right] \times 100\%, \quad (3)$$

Where  $n$  is the refractive index of the filter glass relative to air which can be expressed with schott glass formula as:

$$n = \sqrt{A_0 + A_1 \lambda^2 + A_2 \lambda^{-2} + A_3 \lambda^{-4} + A_4 \lambda^{-6} + A_5 \lambda^{-8}} \quad (4)$$

Where the coefficients for BK7 glass, Silicon dioxide (SiO<sub>2</sub>), Magnesium fluoride (Mg F<sub>2</sub>) are adjusted and recast as shown in Table 1.

Table 1. Schott coefficients for different materials based optical filters [1, 3, 5, 14, 15].

Coefficients	Different materials based Optical filters		
	BK7 glass	Silicon dioxide (SiO <sub>2</sub> )	Magnesium fluoride (Mg F <sub>2</sub> )
A <sub>0</sub>	1.265 (T/T <sub>0</sub> )	0.633 (T/T <sub>0</sub> )	0.48755 (T/T <sub>0</sub> )
A <sub>1</sub>	0.01442 (T/T <sub>0</sub> ) <sup>2</sup>	0.06 (T/T <sub>0</sub> ) <sup>2</sup>	0.04338 (T/T <sub>0</sub> ) <sup>2</sup>
A <sub>2</sub>	1.0032 (T/T <sub>0</sub> )	0.5178 (T/T <sub>0</sub> )	0.39875 (T/T <sub>0</sub> )
A <sub>3</sub>	0.0082 (T/T <sub>0</sub> ) <sup>2</sup>	0.106 (T/T <sub>0</sub> ) <sup>2</sup>	0.0946 (T/T <sub>0</sub> ) <sup>2</sup>
A <sub>4</sub>	0.0543 (T/T <sub>0</sub> )	1.765 (T/T <sub>0</sub> )	2.312 (T/T <sub>0</sub> )
A <sub>5</sub>	41.82 (T/T <sub>0</sub> ) <sup>2</sup>	55.742 (T/T <sub>0</sub> ) <sup>2</sup>	60.706 (T/T <sub>0</sub> ) <sup>2</sup>

The filter absorption coefficient as a function of optical signal wavelength and filter refractive index is [16]:

$$\alpha_\lambda = 10n \left( e^{-0.0458 n \lambda} \right)^2, \text{ cm}^{-1} \quad (5)$$

The reflection loss  $R$  is also dependent on the wavelength and can be calculated as follows [14]:

$$R = \left( \frac{n-1}{n+1} \right)^2 \quad (6)$$

As well as the optical density is the attenuation level also called blocking level which is given by [5, 15]:

$$AL = 10 \log_{10} \left( \frac{1}{T_F} \right), \text{ dB} \quad (7)$$

As optical density increases, the amount of light blocked by the filter (by reflection and/or absorption) increases. The most important point to note is that optical density is

additive. As well as the transmission modulation depth (TMD) is given by [5, 16]:

$$TMD = 10 \log_{10} \left( \frac{1 + \sqrt{P}}{1 - \sqrt{P}} \right), \text{ dB} \quad (8)$$

The optical filtering signal quality, Q can be expressed as a function of operating optical signal wavelength  $\lambda$  and filter full width at half maximum as the following formula [5, 17]:

$$Q = \frac{\lambda}{FWHM} \quad (9)$$

Where FWHM is the full width at half maximum which is applied to such phenomena as the duration of pulse waveforms and the spectral width of sources used for optical communications and the resolution of spectrometers and can be estimated as the following formula [5, 18]:

$$FWHM = 0.635 / BW_f \quad (10)$$

Where  $BW_f$  is the transmitted signal bandwidth with non return to zero coding (NRZ) which is given by [5, 19]:

$$BW_f = \frac{0.7}{\tau} \quad (11)$$

Where  $\tau$  is the total pulse broadening through optical filter which can be given by:

$$\tau = L_f |D_m| \Delta\lambda \quad (12)$$

Where  $L_f$  is the filter length,  $\Delta\lambda$  is the spectral linewidth of the optical source in nm, and  $D_m$  is the material dispersion coefficient based optical filter which can be estimated by:

$$D_m = -\frac{\lambda}{c} \frac{d^2 n}{d\lambda^2}, \quad (13)$$

Where  $c$  is the speed of light ( $3 \times 10^8$  m/sec),  $d^2 n/d\lambda^2$  is the second derivative of filter material refractive index with respect to operating optical signal wavelength  $\lambda$ . Therefore, bit error rate (BER) is considered an important figure of merit for optical signal filtration; all designs are based to adhere to that quality. BER in optical communication system is calculated by the following equation [5, 20]:

$$BER = 0.5 \operatorname{erfc} \left( \frac{Q}{\sqrt{2}} \right) \quad (14)$$

As well as the filter delay time can be estimated by the following equation [5, 18]:

$$\gamma = \frac{n L_f}{c} \quad (15)$$

### III. SIMULATION RESULTS AND PERFORMANCE EVALUATION

Wavelength selective optical filters have been deeply investigated in the ultra violet, visible and near infrared spectrum regions to enhance its performance operation characteristics such as signal filtration quality, filter optical density, filter free spectral range, filter correction factor, and filter transmission modulation depth over wide range of the affecting operating parameters as shown in Table 2.

Table 2. Operating parameters for wavelength selective optical filters [3, 5, 7, 12, 16].

Operating parameter	Symbol	Value
Operating optical signal wavelength in Near infrared region	$\lambda$	1550 nm
Room temperature	$T_0$	25 °C
Filter thickness	$t$	$0.2 \leq t, \text{ mm} \leq 1$
Ambient temperature	$T$	$25 \leq T, \text{ °C} \leq 75$
Spectral linewidth of the optical source	$\Delta\lambda$	0.1 nm
Filter length	$L_f$	20 mm

Based on the modeling equations analysis of advanced glass and plastic optical filters over wide range of the operating parameters, and the series of the Figs. (1-17), the following features are assured:

- i) As shown in Figs. (1-3) have assured that refractive index for different optical filters under study decreases with increasing ambient temperature. Our proposed model have indicated a complete agreement with the experiment results.
- ii) Fig. 4 has indicated that filter signal quality factor decreases with increasing ambient temperature. It is observed that BK7 glass based optical filters has presented the highest signal quality factor in comparison with other materials based optical filters under the same operating conditions.
- iii) As shown in Fig. 5 has assured that filter bandwidth decreases with increasing ambient temperature. It is observed that BK7 glass based optical filters has presented the highest filter bandwidth in comparison with other materials based optical filters under the same operating conditions.
- iv) As shown in Fig. 6 has assured that filter full width at half maximum decreases with increasing ambient temperature. It is indicated that BK7 glass based optical filters has presented the highest filter full width at half maximum in comparison with other materials based optical filters under the same operating conditions.

- v) Fig. 7 has indicated that filter reflection loss increases with increasing ambient temperature. It is observed that BK7 glass based optical filters has presented the lowest filter reflection loss in comparison with other materials based optical filters under the same operating conditions.
- vi) As shown in Fig. 8 has assured that filter correlation factor decreases with increasing ambient temperature. It is indicated that BK7 glass based optical filters has presented the highest filter correlation factor in comparison with other materials based optical filters under the same operating conditions.
- vii) Fig. 9 has demonstrated that filter bit error rate increases with increasing ambient temperature. It is observed that BK7 glass based optical filters has presented the lowest filter bit error rate in comparison with other materials based optical filters under the same operating conditions.
- viii) Figs. (10-12) have assured that filter transmission decreases with increasing both ambient temperature and filter thickness. It is observed that BK7 glass based optical filters has presented the highest filter transmission in comparison with other materials based optical filters under the same operating conditions.
- ix) Fig. 13. has demonstrated that filter modulation depth decreases with increasing both ambient temperature and filter thickness. It is observed that BK7 glass based optical filters has presented the highest filter modulation depth in

comparison with other materials based optical filters under the same operating conditions.

- x) Fig. 14 has indicated that filter delay time increases with increasing ambient temperature. It is observed that BK7 glass based optical filters has presented the lowest filter delay time in comparison with other materials based optical filters under the same operating conditions.
- xi) Figs. (15-17) have assured that filter attenuation level increases with increasing both ambient temperature and filter thickness. It is observed that BK7 glass based optical filters has presented the lowest filter attenuation level in

comparison with other materials based optical filters under the same operating conditions.

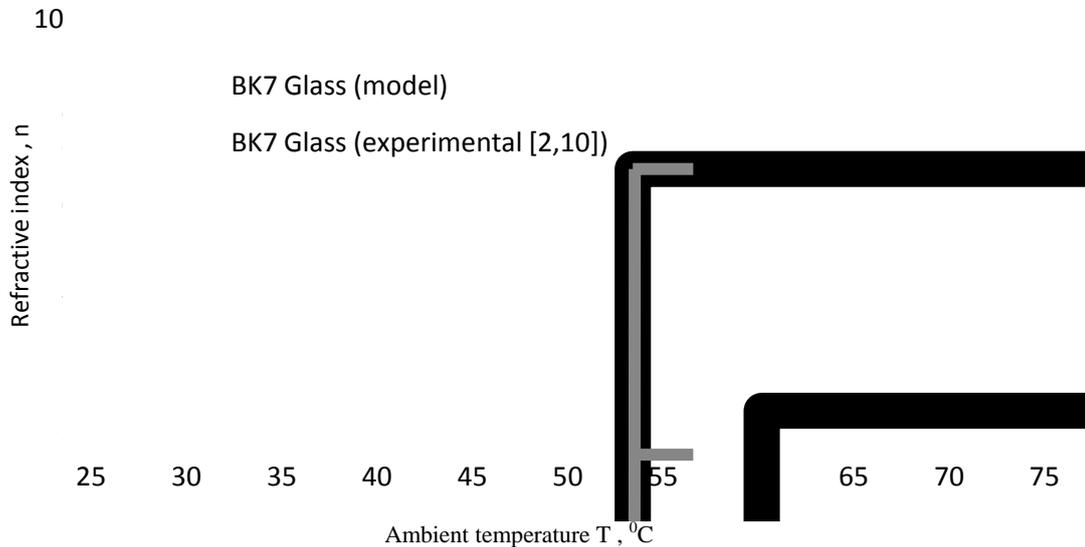


Fig.1. Refractive index variations of BK7 glass filter with ambient temperature variations for both our proposed model and their experimental data under the assumed set of the operating parameters.

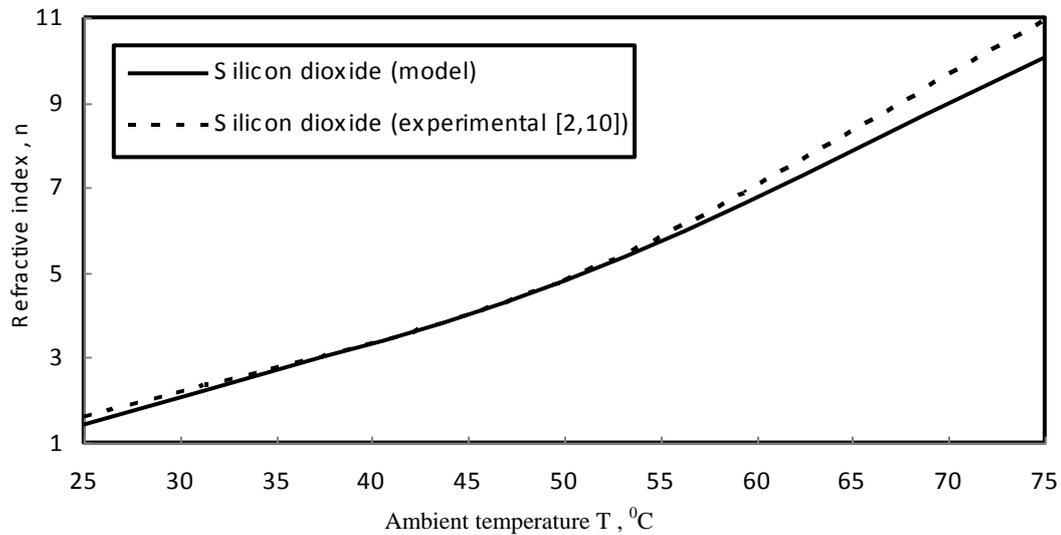


Fig. 2. Refractive index variations of silicon dioxide filter with ambient temperature variations for both our proposed model and their experimental data under the assumed set of the operating parameters.

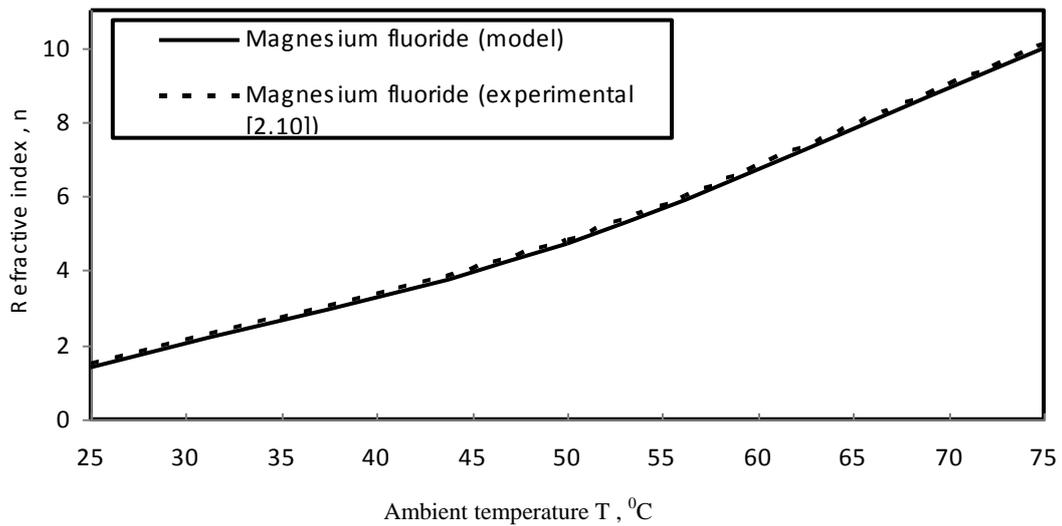


Fig. 3. Refractive index variations of magnesium fluoride filter with ambient temperature variations for both our proposed model and their experimental data under the assumed set of the operating parameters.

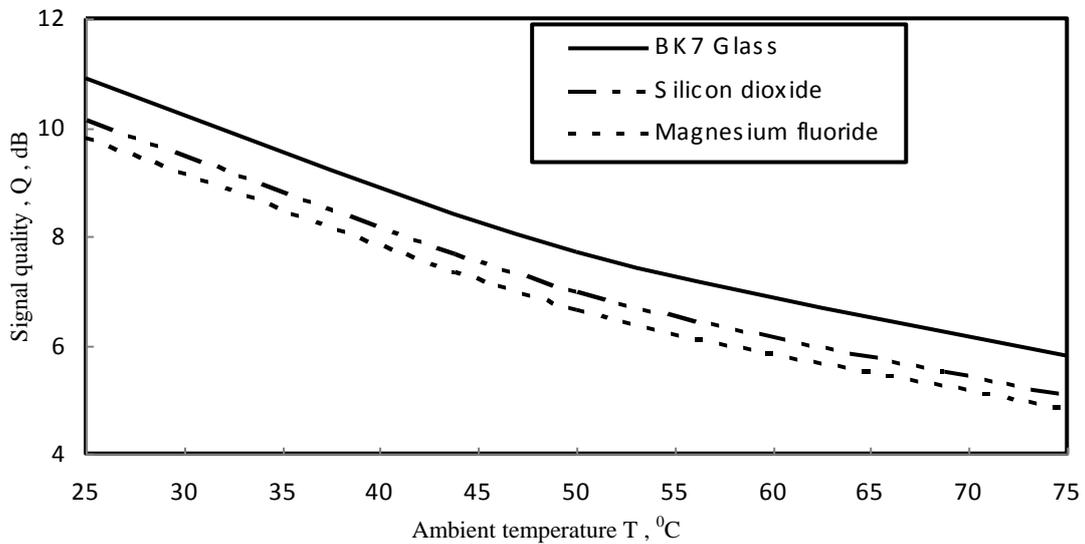


Fig.4. Signal quality factor in relation to ambient temperature for different optical filters under the assumed set of the operating parameters.

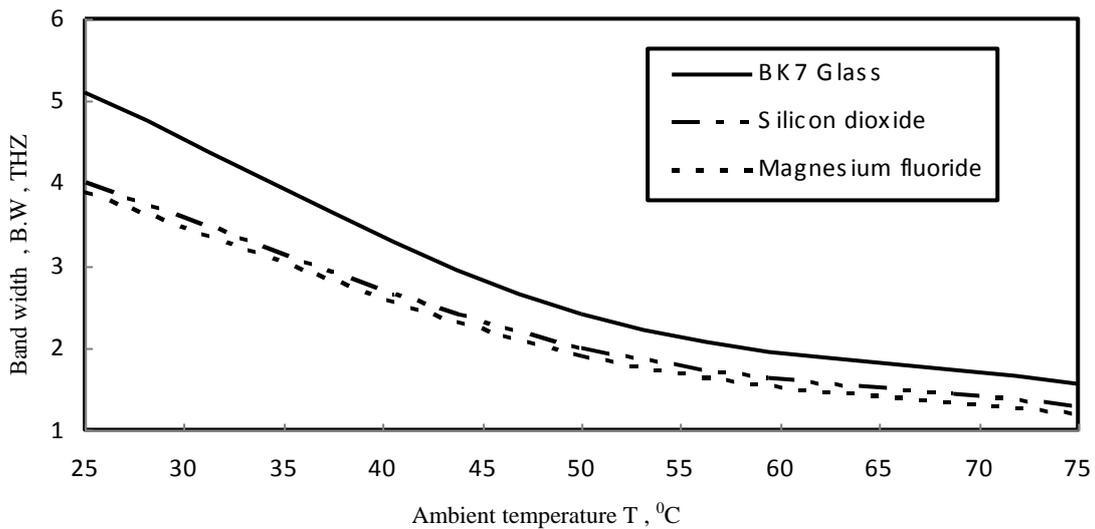


Fig.5. Band width in relation to ambient temperature for different optical filters under the assumed set of the operating parameters.

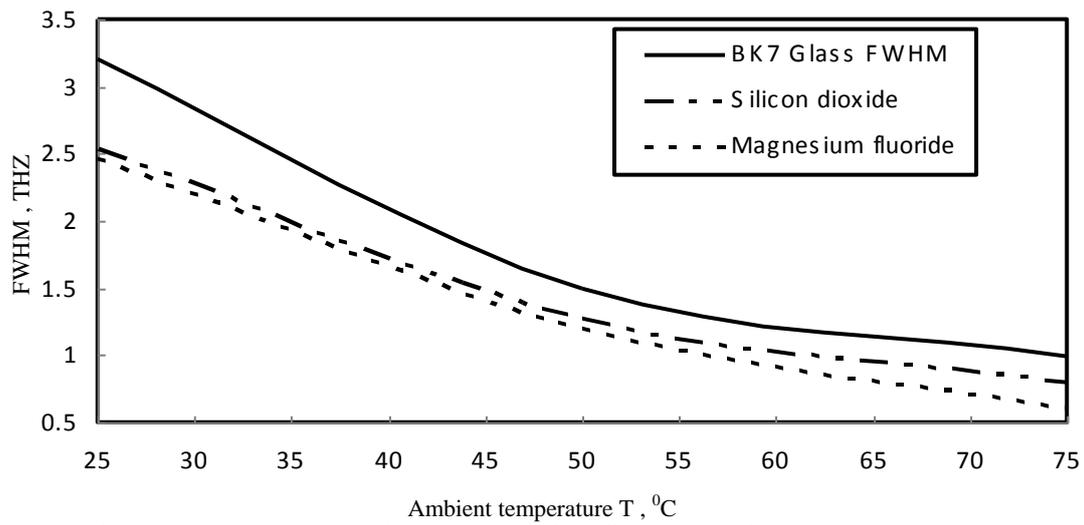


Fig. 6. Full width at half maximum in relation to ambient temperature for different optical filters under the assumed set of the operating parameters.

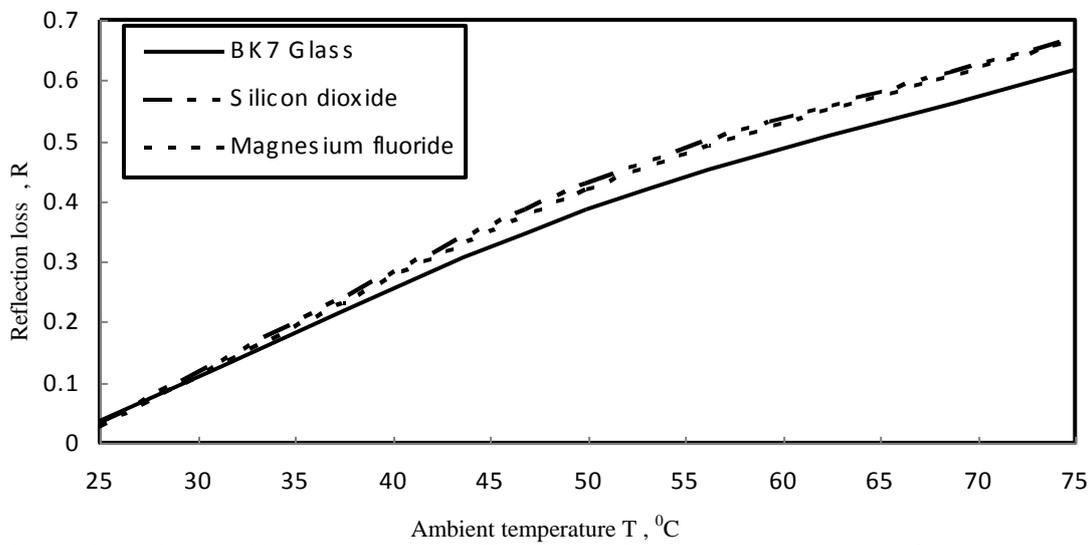


Fig. 7. Reflection loss in relation to ambient temperature for different optical filters under the assumed set of the operating parameters.

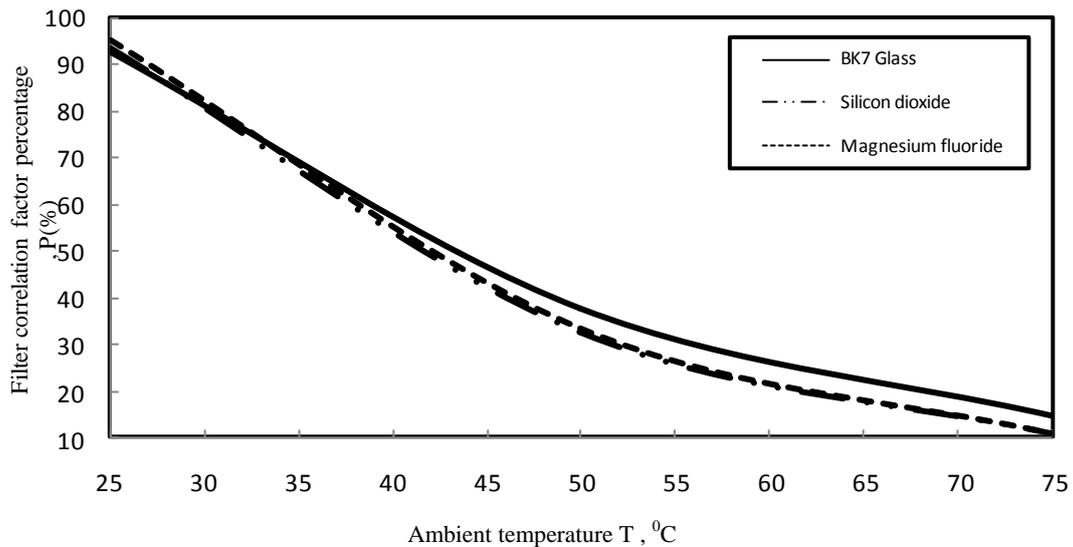


Fig. 8. Filter correction factor percentage in relation to ambient temperature for different optical filters under the assumed set of the operating parameters.

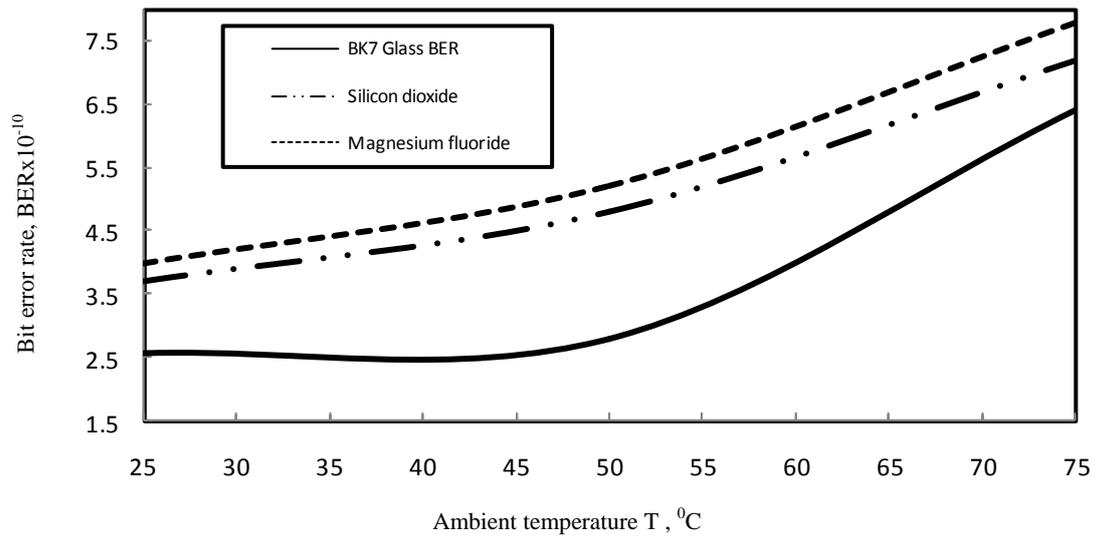


Fig. 9. Bit error rate in relation to ambient temperature for different optical filters under the assumed set of the operating parameters.

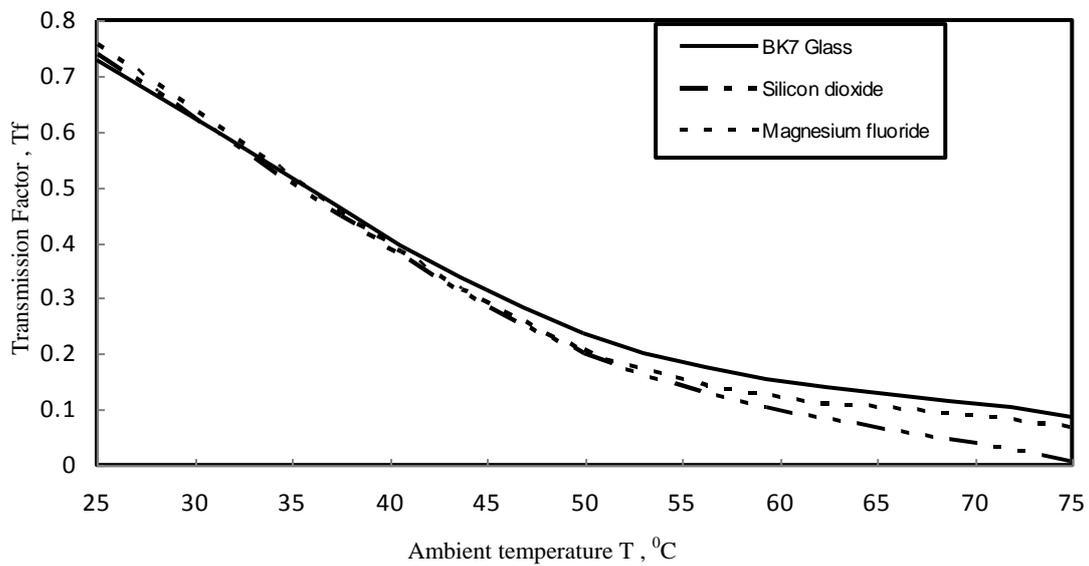


Fig.10. Transmission factor with filter thickness 0.2 mm in relation to ambient temperature for different optical filters under the assumed set of the operating parameters.

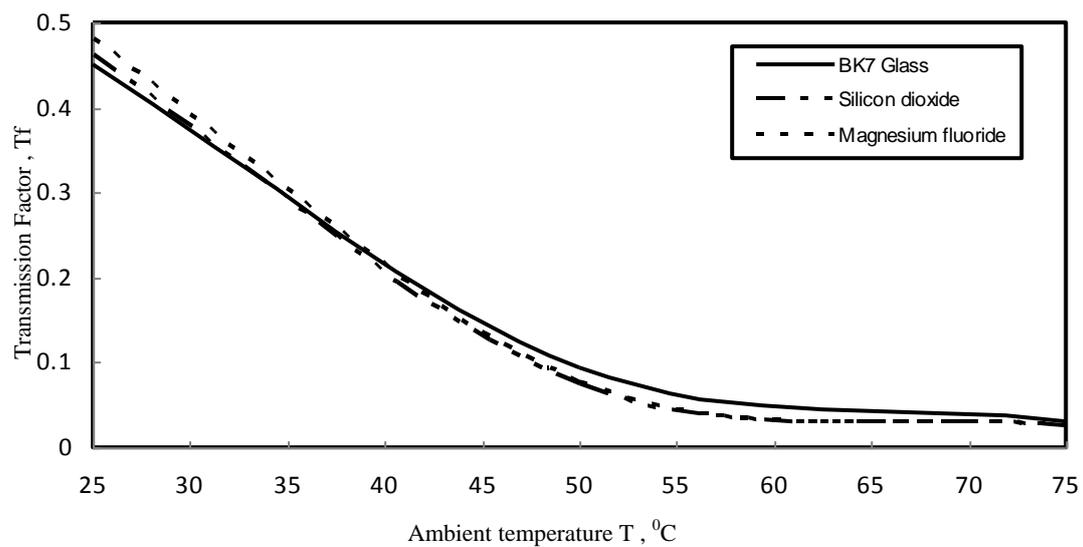


Fig.11. Transmission factor with filter thickness 0.6 mm in relation to ambient temperature for different optical filters under the assumed set of the operating parameters.

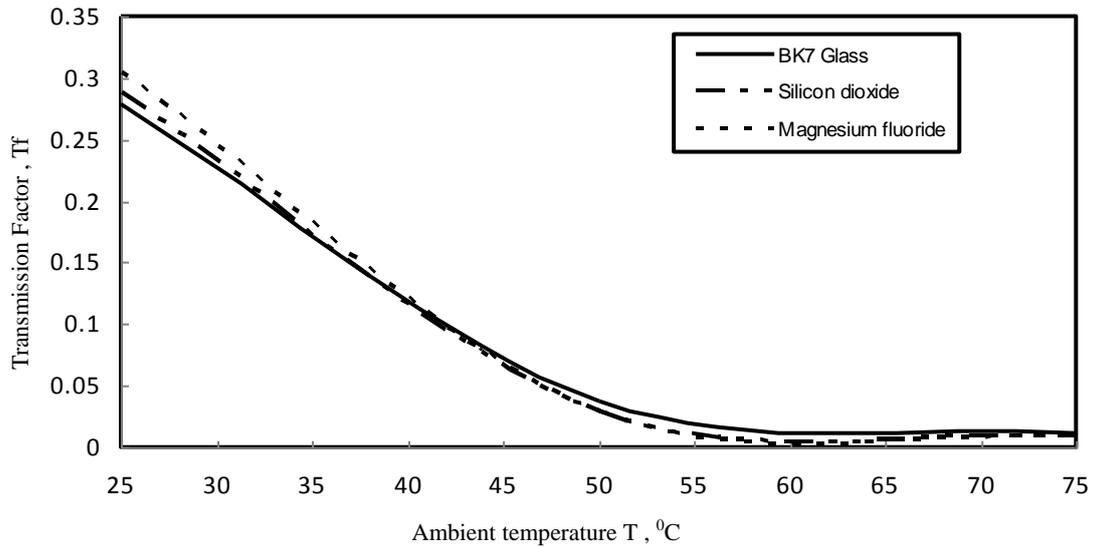


Fig.12. Transmission factor with filter thickness 1 mm in relation to ambient temperature for different optical filters under the assumed set of the operating parameters.

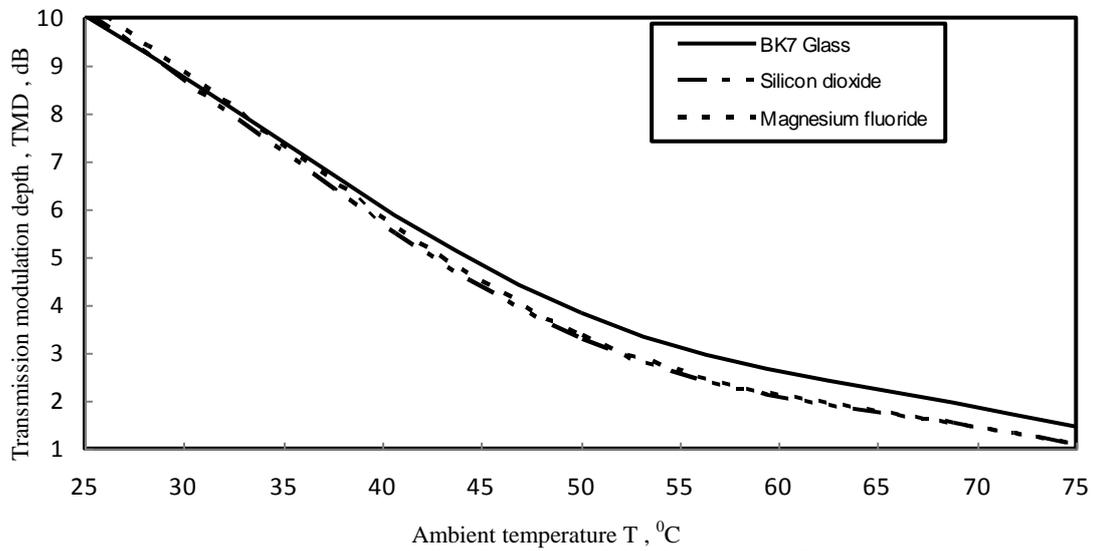


Fig. 13. Transmission modulation depth in relation to ambient temperature for different optical filters under the assumed set of the operating parameters.

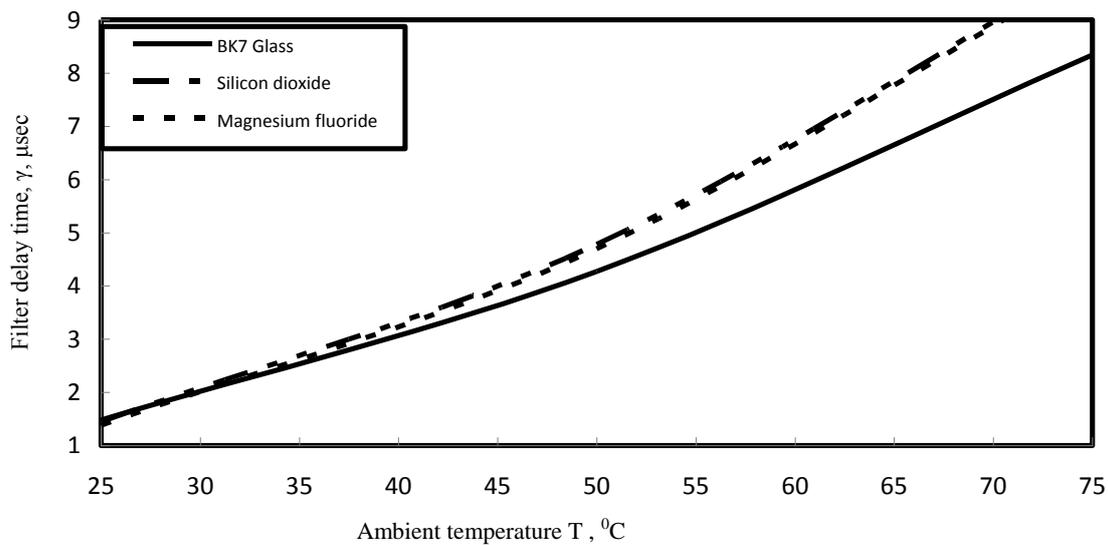


Fig. 14. Filter delay time in relation to ambient temperature for different optical filters under the assumed set of the operating parameters.

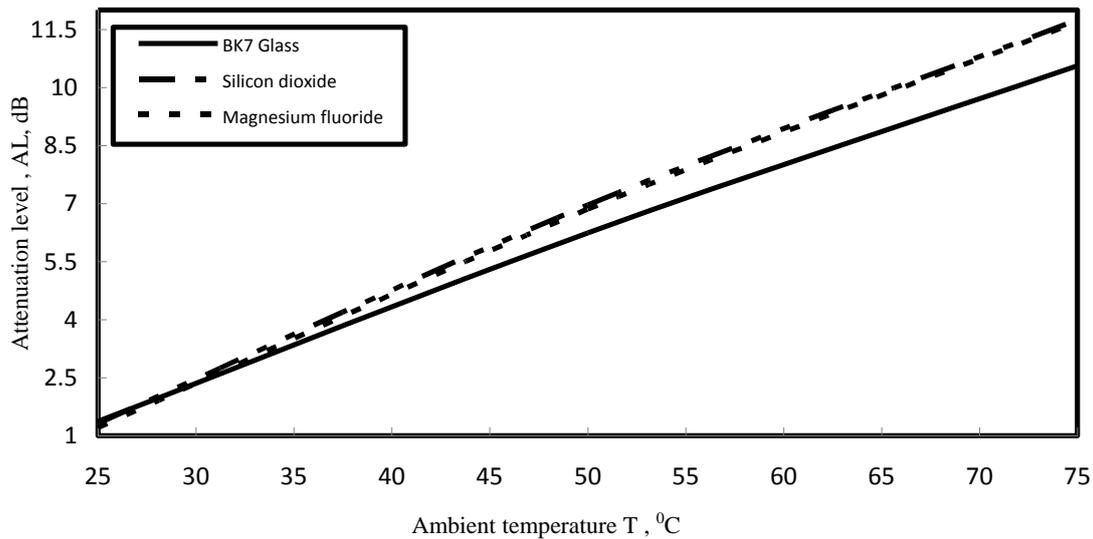


Fig. 15. Attenuation level with filter thickness 0.2 mm in relation to ambient temperature for different optical filters under the assumed set of the operating parameters.

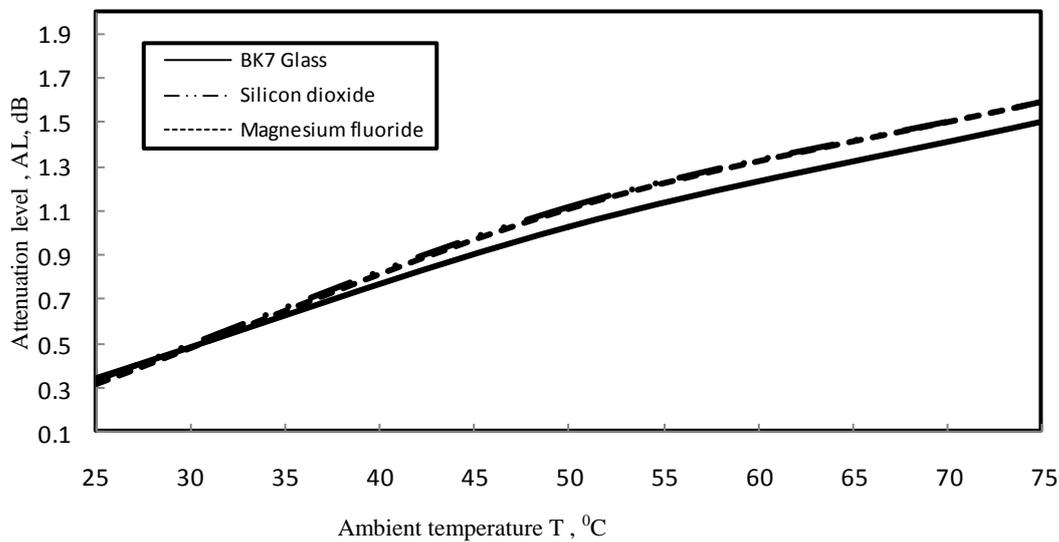


Fig. 16. Attenuation level with filter thickness 0.6 mm in relation to ambient temperature for different optical filters under the assumed set of the operating parameters.

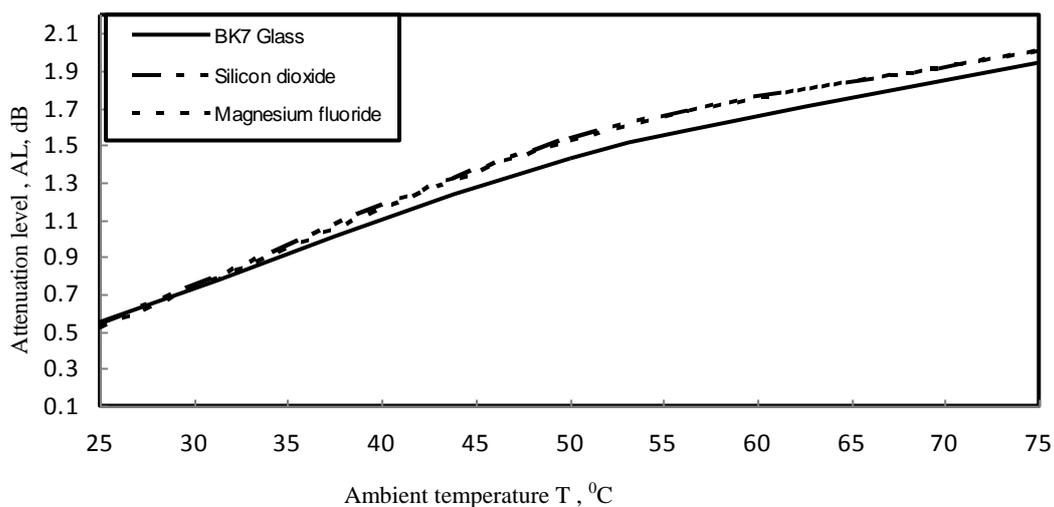


Fig. 17. Attenuation level with filter thickness 1 μm in relation to ambient temperature for different optical filters under the assumed set of the operating parameters.

#### IV. CONCLUSIONS

In a summary, we have deeply investigated the optical signal filtering processing for signal quality testing in optical fiber communication systems. It is theoretically found that the harmful

high thermal and increased filter thickness effects on the optical filter transmission performance efficiency. As well as it is observed that BK7 glass optical filter has presented the highest signal quality, signal transmission, filter correlation factor, transmission modulation depth and filter bandwidth and the lowest filter bit

error, filter delay time, reflection loss, and filter attenuation level. Thus BK7 glass optical filter is the best candidate for optical filters among proposed optical filters under study under the same thermal effects and third window transmission spectral operating conditions. It is indicated that the dramatic thermal effects on the optical filter transmission performance efficiency.

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