

# RLC Low Pass Filters Transmission Transient Performance Characteristics Analysis

Ahmed Nabih Zaki Rashed

Electronics and Electrical Communications Engineering Department  
Faculty of Electronic Engineering, Menouf 32951, Menoufia University, EGYPT  
E-mail: ahmed\_733@yahoo.com

**Abstract**— Filter is considered as a part of an optical system that has the purpose of modifying the intensity, polarization or, in particular, the spectral distribution of light. For reconfigurable filters a signal is applied to tune the filter's properties or change between different configurations. Filters of some sort are essential to the operation of most electronic circuits. It is therefore in the interest of anyone involved in electronic circuit design to have the ability to develop filter circuits capable of meeting a given set of specifications. delay time steady state error, operating frequency, and wavelength, damping frequency, and wavelength the major interesting design parameters for different categories of signal filtering under operation considerations.

**Keywords**— Time response, steady state error, steady state output, Low pass filter, and Peak Time.

## I. INTRODUCTION

Examples of new sources include more efficient mid ultra violet (UV) lasers, and more conventional broadband sources such as high pressure mercury and xenon arc lamps with improved efficiency and longer lifetimes [1, 2]. A major impediment that continues to make the mid-UV an optically challenging spectral region is the lack of durable optical filters with adequate performance. However, optical filters constructed from thin-film coating materials that have relatively low absorption and spectral dispersion yet high reliability at these short wavelengths would have significant advantages over components such as the diffraction gratings used in monochromators and spectrophotometers. In general, grating-based systems are not as selective and do not achieve as much throughput as filter based systems, and only filters allow direct imaging [3]. Until recently, optical filters for the mid-UV have exhibited poor performance in terms of transmission, spectral selectivity and durability. Optical filters made with soft-coated thin-film materials and/or multiple laminated absorbing and transparent glass substrates cannot withstand the intense energies of illumination at mid-UV wavelengths [4].

Hybrid metal dielectric filters also have poor optical damage thresholds, and inadequately low transmission and edge steepness. Optical filters with good performance in the mid-UV are crucial for enabling important new instruments based on applications including biochemical absorption, fluorescence and spectroscopy, as well as for realizing the full potential of industrial applications in areas including semiconductor and electronics manufacturing [5-7].

## II. FILTER MODELING ANALYSIS

### II. 1. RLC LOW PASS FILTER

RLC low pass Filters can be designed by using inductors, capacitors and resistors as shown in Fig. 1. RLC low pass filters output is taken from capacitor side.

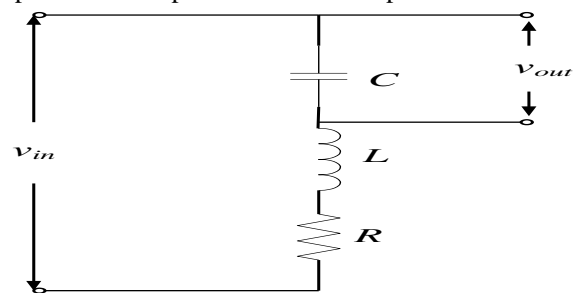


Fig. 1. An RLC low pass filter.

The RLC low pass filter (LPF) transfer function (Gain) can be expressed as the following formula [8]:

$$\frac{v_{out}}{v_{in}} = \frac{\frac{1}{SC}}{SL + \frac{1}{SC} + R} = \frac{1}{S^2LC + 1 + SRC} = \frac{\frac{1}{LC}}{S^2 + S\frac{R}{L} + \frac{1}{LC}} \quad (1)$$

If the input is unit step function, then the output as a function of time constant (t) can be expressed as:

$$v_{out}(t) = \frac{e^{-\frac{\xi}{\sqrt{LC}}t}}{\sqrt{1-\xi^2}} \sin(f_d t + \phi) \quad (2)$$

Where  $f_d$  is the damping frequency,  $\phi$  is the phase shift,  $\xi$  is the damping ratio, and time constant, t can be expressed as:

$$t = \sqrt{LC} \quad (3)$$

Based on the second order filter circuit, the operating frequency,  $f_0$ , and damping frequency,  $f_d$  can be given by:

$$f_0 = \frac{R}{2\xi\sqrt{LC}} \quad (4)$$

$$f_d = f_0\sqrt{1-\xi^2} \quad (5)$$

As well as the phase shift of filter circuit,  $\phi$  can be expressed as the following formula [9]:

$$\phi = \tan^{-1}\left(\frac{\sqrt{1-\xi^2}}{\xi}\right) \quad (6)$$

The rise time  $T_r$ , and settling time  $T_s$ , of the filter circuit can be given by [10]:

$$T_r = \frac{1}{f_d} \tan^{-1}\left(\frac{1-\xi^2}{\xi}\right) \quad (7)$$

$$T_s = \frac{4}{\xi f_0} \quad (8)$$

In the same way, the delay and peak times,  $T_d$ , and  $T_p$  are described by the following expressions [11]:

$$T_d = \frac{1+0.7 \xi}{f_0} \tag{9}$$

$$T_p = \frac{\pi}{f_0 \sqrt{1-\xi^2}} = \frac{\pi}{f_d} \tag{10}$$

The percentage steady state error of the RLC low pass filter circuit can be described as the following formula [12]:

$$E_{ss}(\%) = \frac{1}{1+\sqrt{LC}} \times 100\% \tag{11}$$

Where inductance (L) and capacitance (C) in this relation in  $\mu\text{H}$  and nF respectively.

### III. PERFORMANCE ANALYSIS

RLC low filters have been deeply investigated under damped conditions to enhance it performance operation characteristics such as steady state error, rose time, peak time, settling time and delay time over wide range of the affecting operating parameters as shown in Table 1.

Table 1. Operating parameters for Electrical Filters [3, 5, 11, 13].

Operating parameter	Symbol	Value
Resistance	R	10 K $\Omega$ -100 K $\Omega$
Inductance	L	0.1 $\mu\text{H}$ - 1 $\mu\text{H}$
Capacitance	C	10 nF-100 nF
Damping ratio	$\xi$	0.2-0.9

Based on the modeling equations analysis over wide range of the operating parameters, and the series of the Figs. (1-19), the following features are assured:

- i) Figs. (1-4) have assured that the resonance frequency is inversely proportional to capacitance and inductance, when capacitance and inductance increase this leads to the resonance frequency decreases. As well as, when the damping ratio increases this leads to the Resonance frequency ( $f_0$ ) decreases at the assumed set of operating parameter.

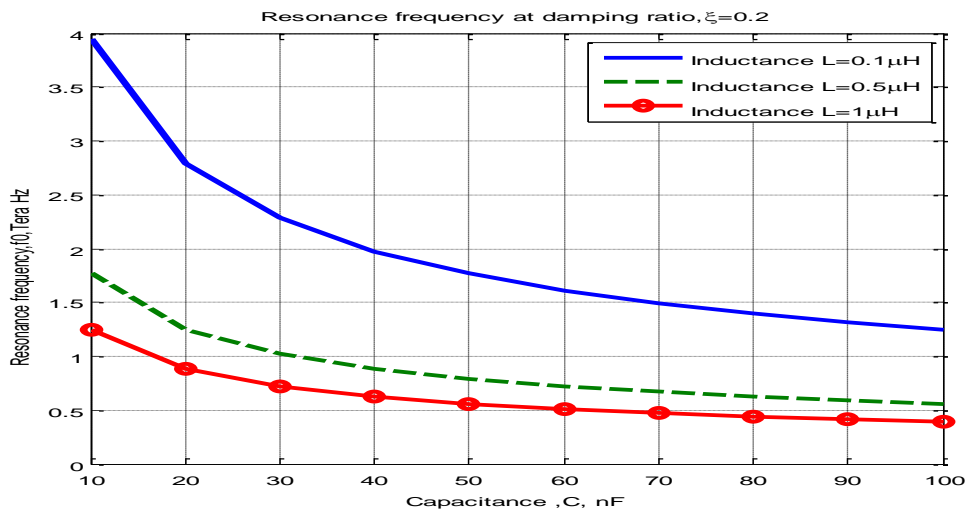


Fig . 1. variation of resonance frequency  $f_0$  against variation of capacitance with inductance at  $\xi = 0.2$  assumed set of the operating parameters

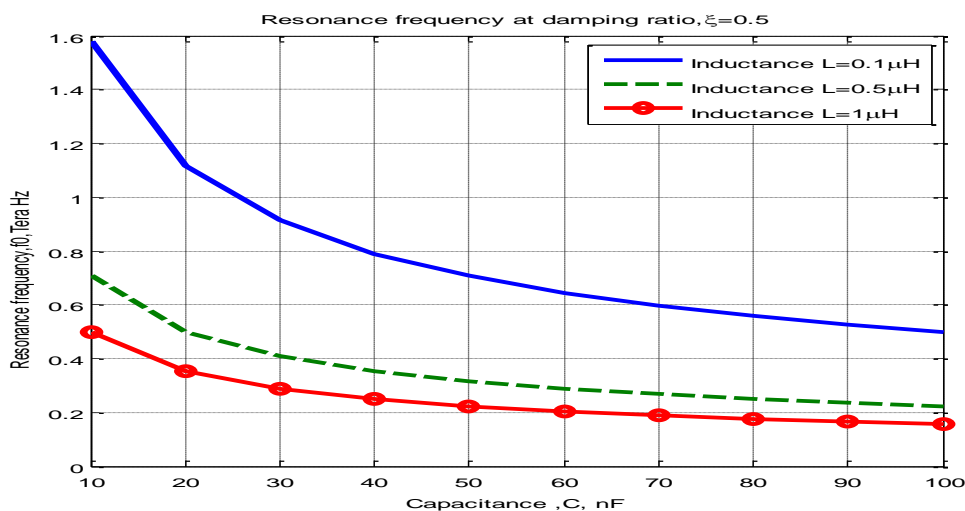


Fig . 2. . variation of resonance frequency  $f_0$  against variation of capacitance with inductance at  $\xi = 0.5$  assumed set of the operating parameters

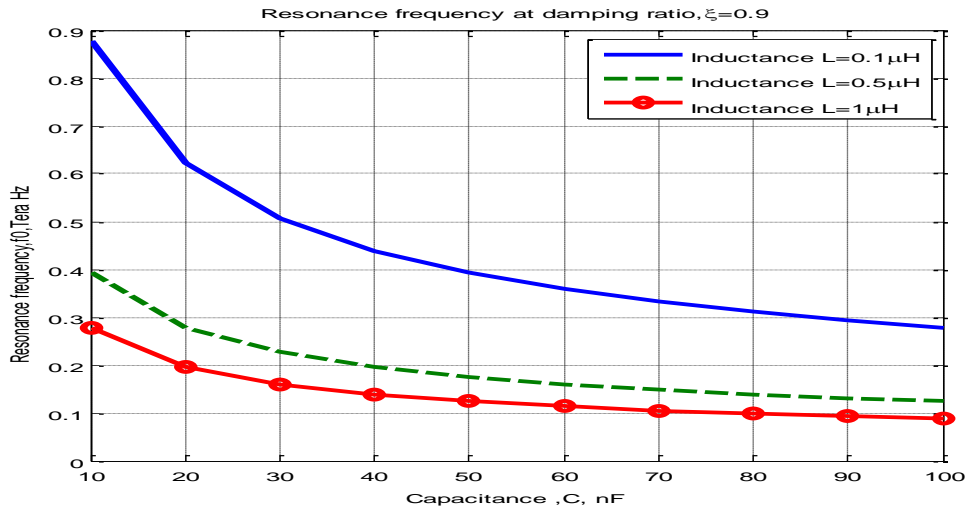


Fig .3. variation of resonance frequency  $f_0$  against variation of capacitance with inductance at  $\xi=0.9$  assumed set of the operating parameters

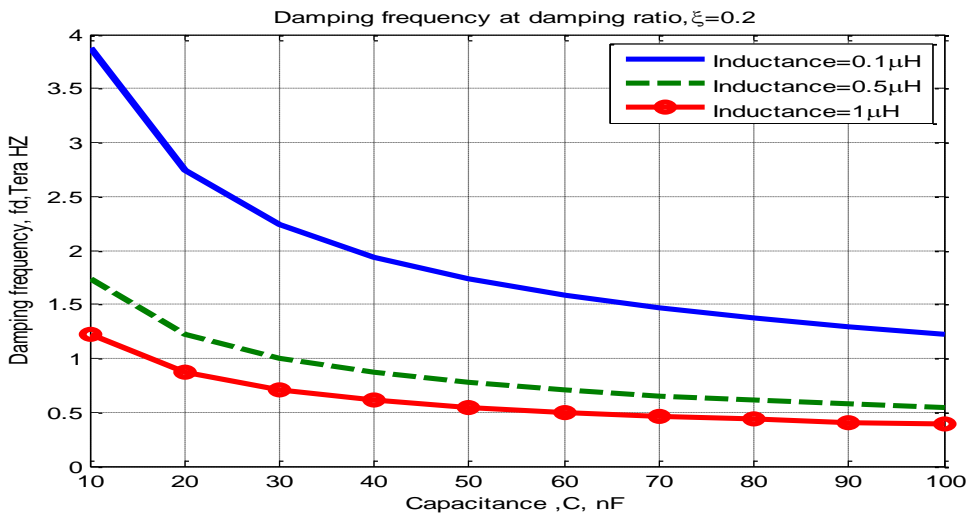


Fig .4. variation of damping frequency  $f_d$  against variation of capacitance with inductance at  $\xi=0.2$  assumed set of the operating parameters

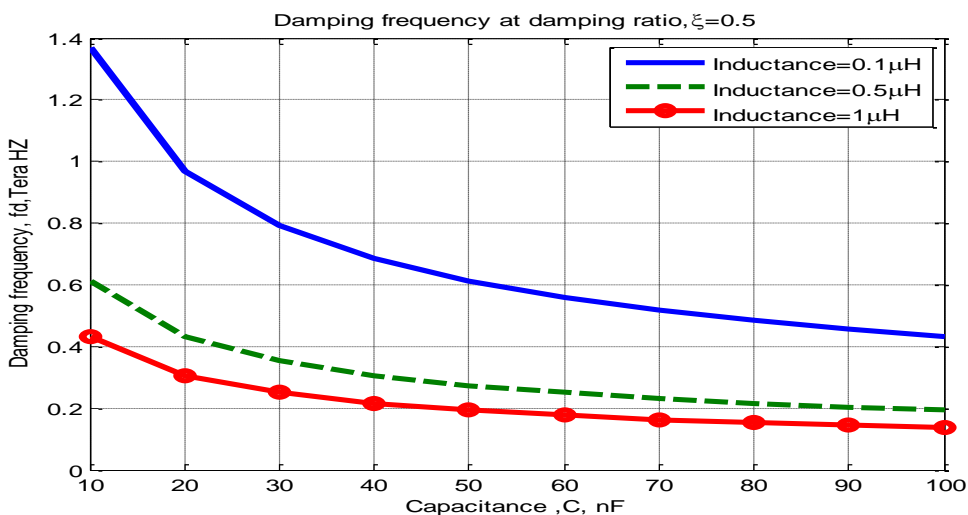


Fig .5. variation of damping frequency  $f_d$  against variation of capacitance with inductance at  $\xi=0.5$  assumed set of the operating parameters

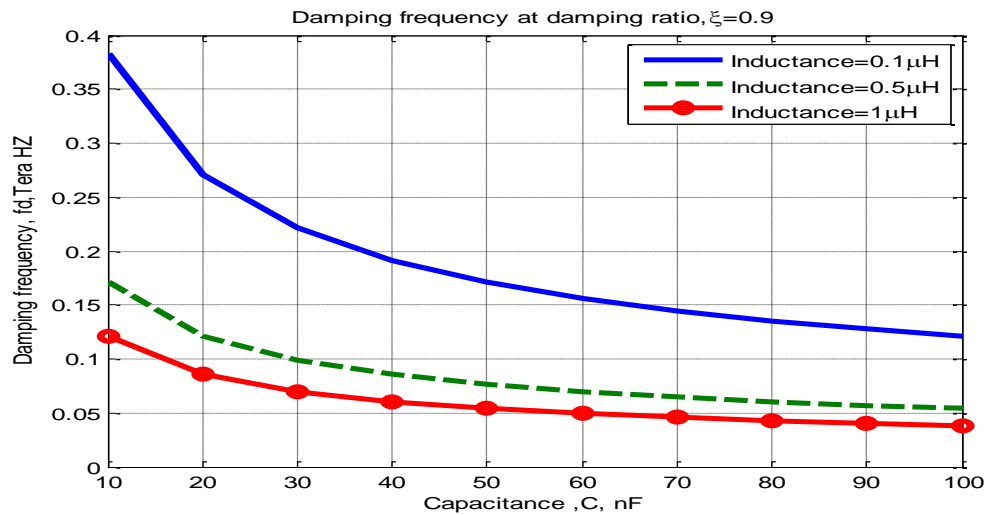


Fig .6. variation of damping frequency  $f_d$  against variation of capacitance with inductance at  $\xi = 0.9$  assumed set of the operating parameters

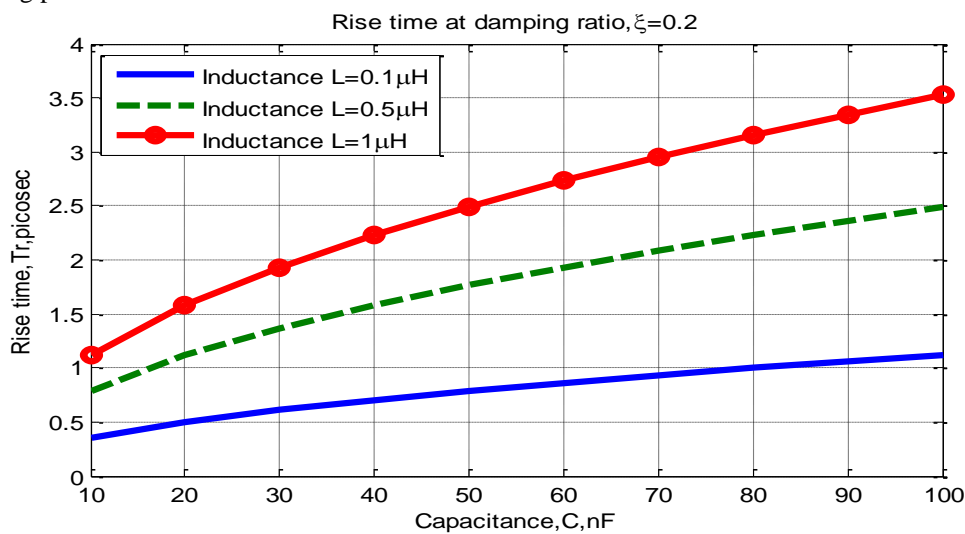


Fig .7. variation of Rise time  $T_r$  against variation of capacitance with inductance at  $\xi = 0.2$  assumed set of the operating parameters

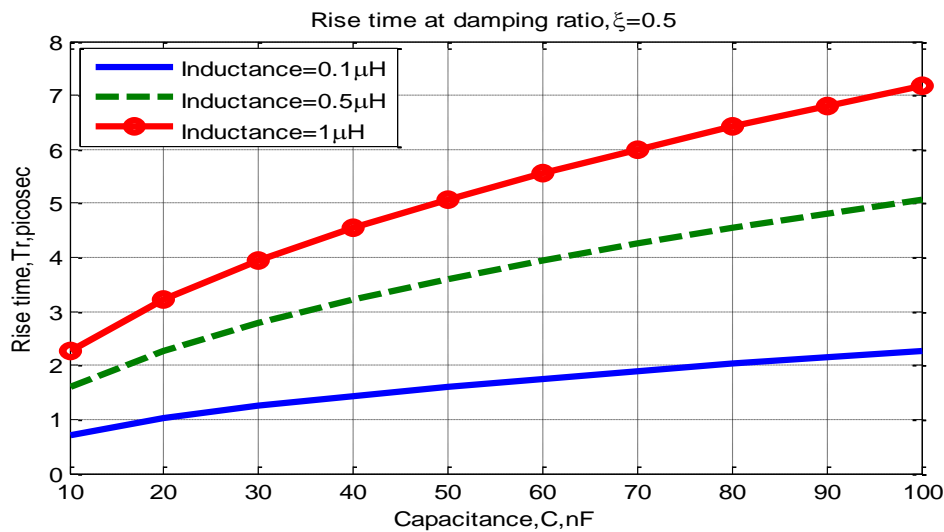


Fig .8. variation of Rise time  $T_r$  against variation of capacitance with inductance at  $\xi = 0.5$  assumed set of the operating parameters

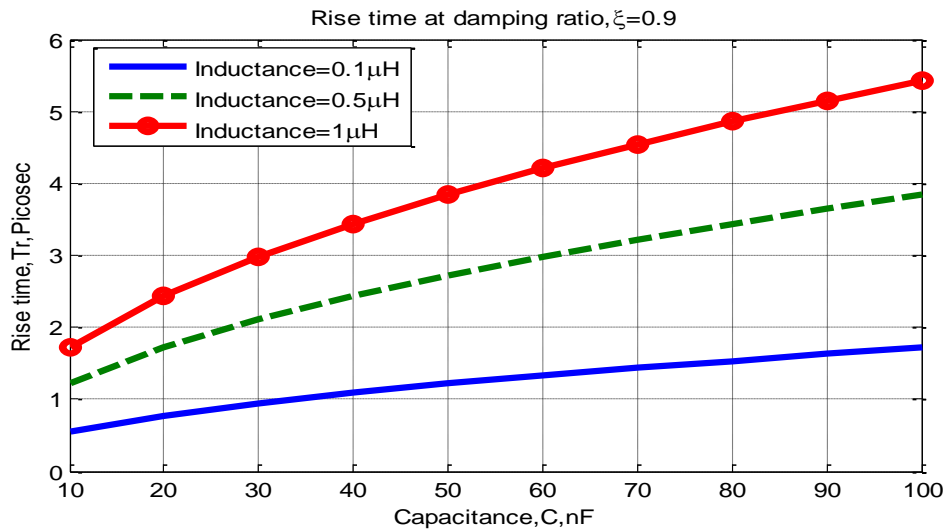


Fig .9. variation of Rise time  $T_r$  against variation of capacitance with inductance at  $\xi =0.9$  assumed set of the operating parameters

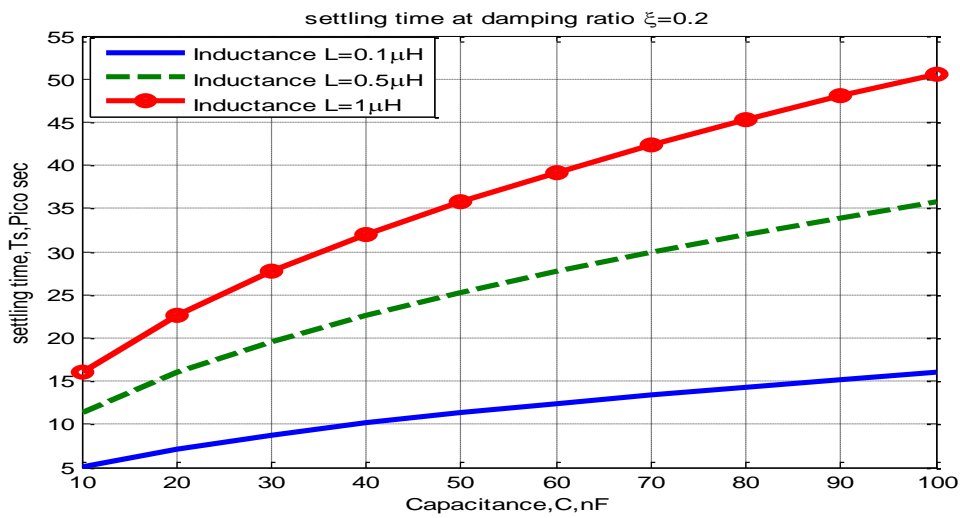


Fig .10. Variation of settling time  $T_s$  against variation of capacitance with inductance at  $\xi =0.2$  assumed set of the operating parameters

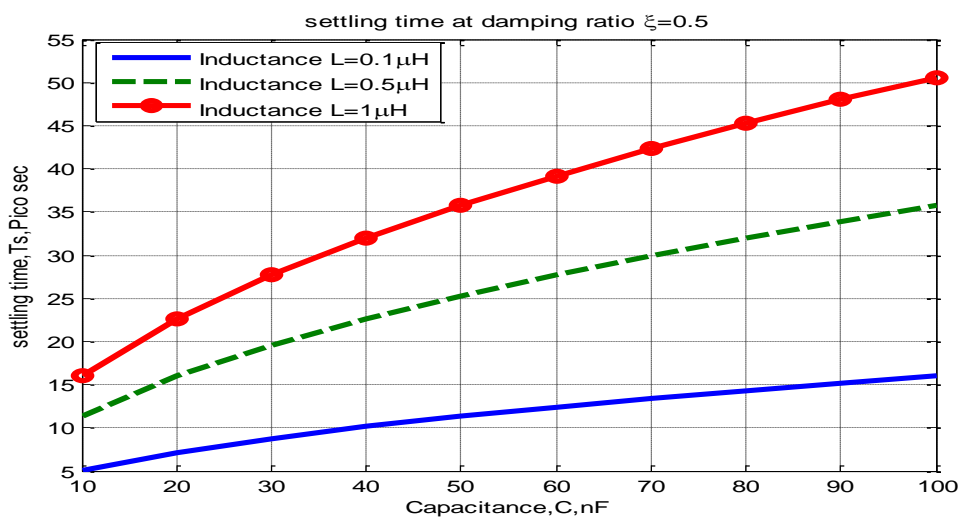


Fig .11. variation of settling time  $T_s$  against variation of capacitance with inductance at  $\xi =0.5$  assumed set of the operating parameters

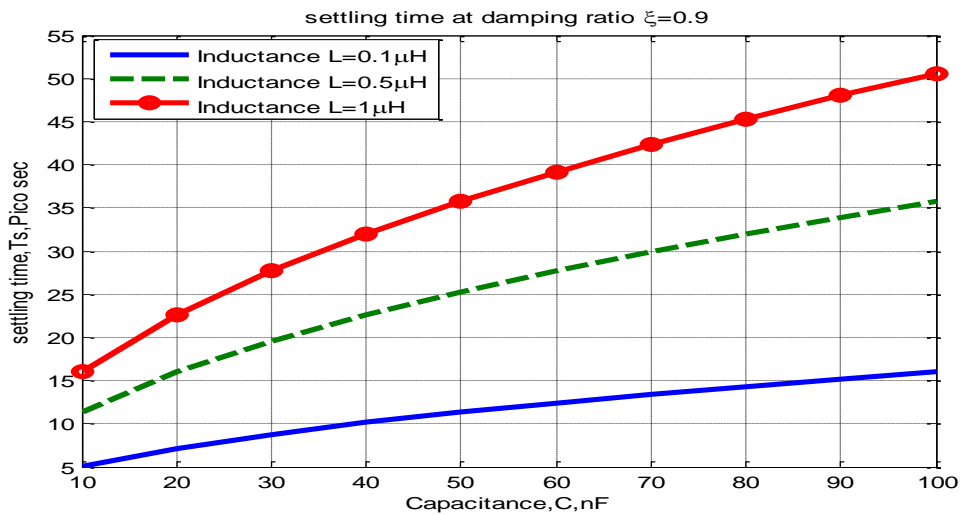


Fig .12. variation of settling time  $T_s$  against variation of capacitance with inductance at  $\xi=0.9$  assumed set of the operating parameters

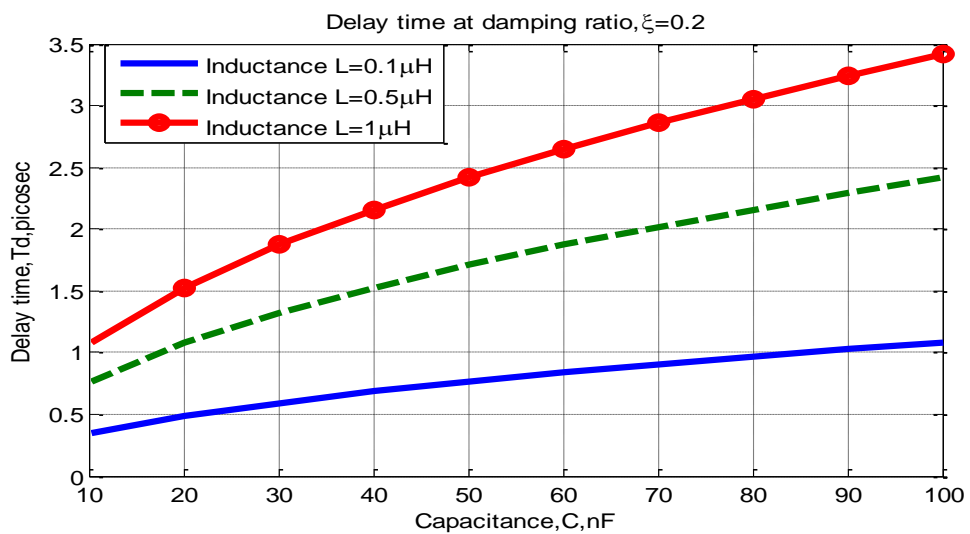


Fig .13. variation of delay time  $T_d$  against variation of capacitance with inductance at  $\xi=0.2$  assumed set of the operating parameters

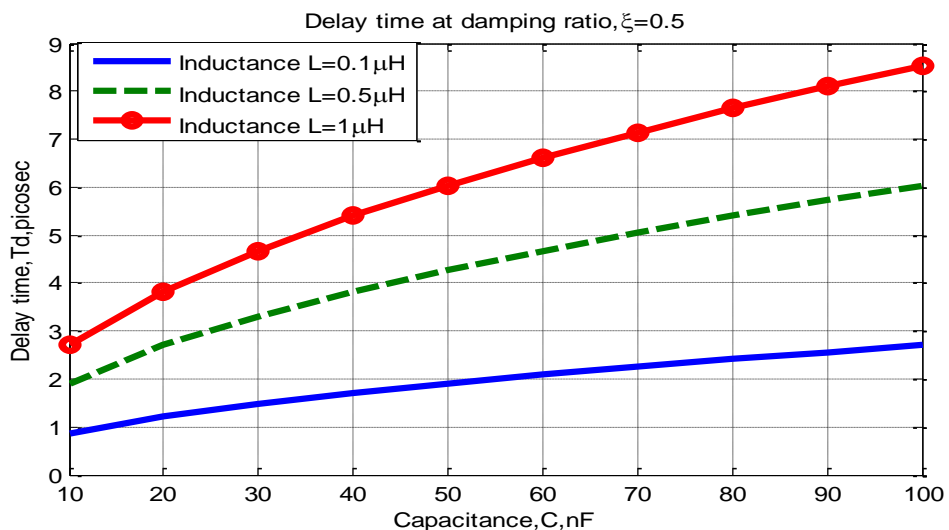


Fig .14. variation of delay time  $T_d$  against variation of capacitance with inductance at  $\xi=0.5$  assumed set of the operating parameters

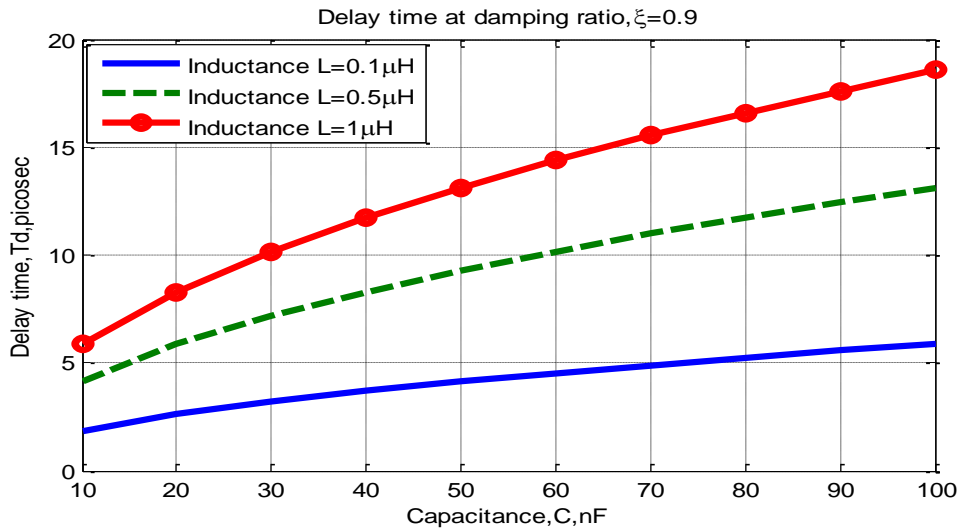


Fig .15. variation of delay time  $T_d$  against variation of capacitance with inductance at  $\xi =0.9$  assumed set of the operating parameters

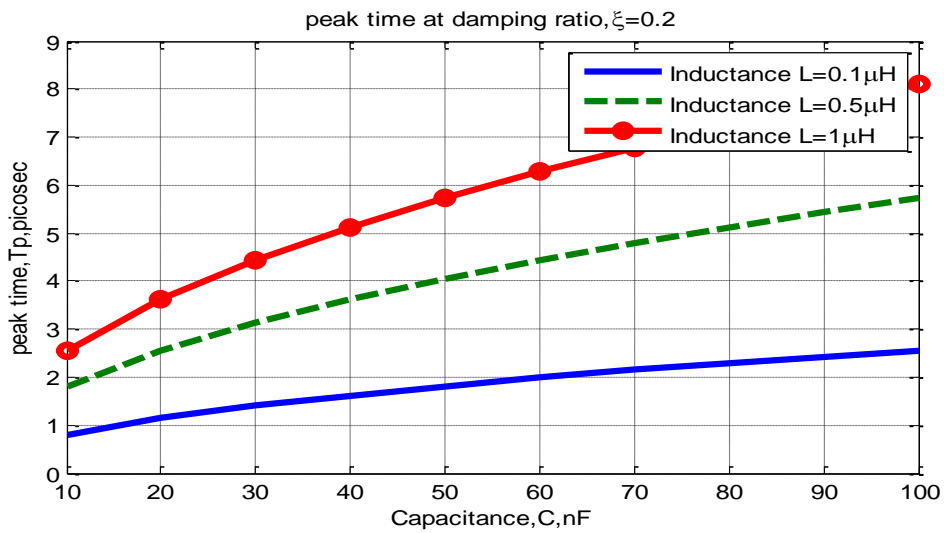


Fig .16. variation of peak time  $T_p$  against variation of capacitance with inductance at  $\xi =0.2$  assumed set of the operating parameters

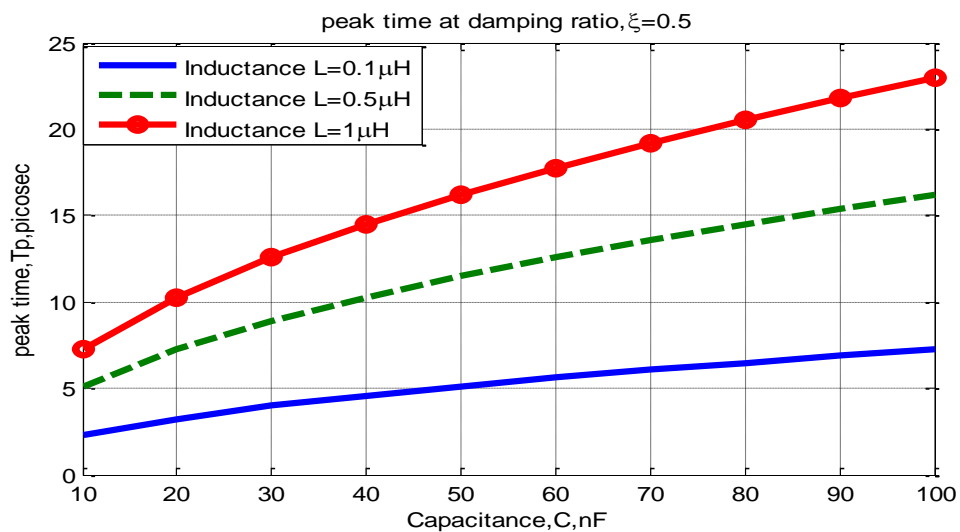


Fig .17. variation of peak time  $T_p$  against variation of capacitance with inductance at  $\xi =0.5$  assumed set of the operating parameters

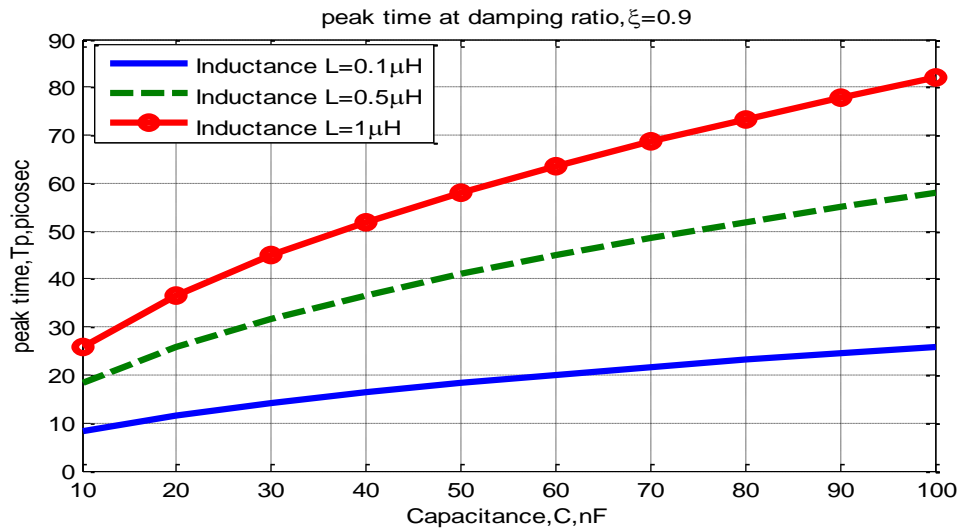


Fig .18. variation of peak time Tp against variation of capacitance with inductance at  $\xi = 0.9$  assumed set of the operating parameters

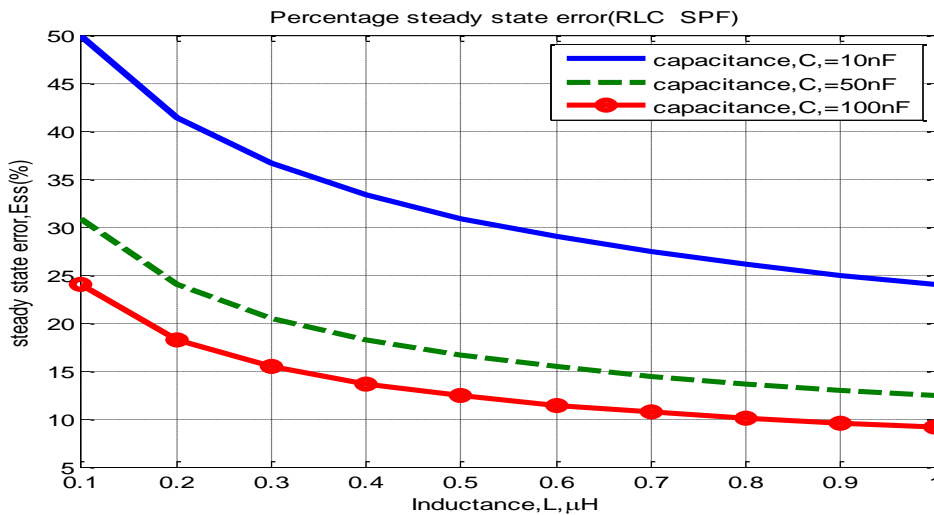


Fig .19. variation of steady state error [Ess] against variation of inductance with capacitance at the assumed set of the operating parameters

- ii) Figs. (5-8) have assured that Rise time ( $T_r$ ) is directly proportional to capacitance and inductance. As well as when damping ratio increases this leads to the Rise time increases, at the assumed set of operating parameter.
- iii) Figs. (9-11) have assured that settling time ( $T_s$ ) is directly proportional to capacitance and inductance. As well as when damping ratio increases this leads to the settling time increases at the assumed set of operating parameter.
- iv) Figs. (12-15) have assured that Delay time ( $T_d$ ) is directly proportional to capacitance and inductance. As well as when damping ratio increases this leads to the Delay time increases, at the assumed set of operating parameter.
- v) Figs. (16-18) have assured that peak time ( $T_p$ ) is directly proportional to capacitance and inductance. As well as when damping ratio increases this leads to the Peak time increases, at the assumed set of operating parameter.
- vi) Fig. (19) has assured that the steady state error is inversely proportional to capacitance and inductance circuit components at the assumed set

of operating parameter.

#### IV. CONCLUSIONS

In a summary, when the capacitance and resistance increase, then resonance frequency ( $f_0$ ) and damping frequency ( $f_d$ ) decrease. As well as it is theoretically found that when the capacitance and resistance increase then rise time( $T_r$ ), settling time( $T_s$ ), Delay time( $T_d$ ) and peak time( $T_p$ ) increase. Transient time response operation performance of RLC low pass filters for under damped systems conditions are shown in Table 2.

Table 2: Transient Time response of RLC filters over under damped conditions.

Transient time response design parameters	RLC low pass filter		
	$\xi=0.2$	$\xi=0.5$	$\xi=0.9$
Operating frequency, $f_0$ , THz	3.95	1.58	0.8
Damping frequency, $f_d$ , THz	3.87	1.37	0.3
Rise time, $T_r$ , psec	0.2	0.7	0.5
Settling time, $T_s$ , psec	5	5.1	5.5
Delay time, $T_d$ , psec	0.2	0.85	2
Peak time, $T_p$ , psec	0.8	2.3	9



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## Author's Profile



**Dr. Ahmed Nabih Zaki Rashed** was born in Menouf city, Menoufia State, Egypt country in 23 July, 1976. Received the B.Sc., M.Sc., and Ph.D. scientific degrees in the Electronics and Electrical Communications Engineering Department from Faculty of Electronic Engineering, Menoufia University in 1999, 2005, and 2010 respectively. Currently, his job carrier is a scientific lecturer in Electronics and Electrical Communications Engineering Department, Faculty of Electronic Engineering, Menoufia university, Menouf.

Postal Menouf city code: 32951, EGYPT. His scientific master science thesis has focused on polymer fibers in optical access communication systems. Moreover his scientific Ph. D. thesis has focused on recent applications in linear or nonlinear passive or active in optical networks. His interesting research mainly focuses on transmission capacity, a data rate product and long transmission distances of passive and active optical communication networks, wireless communication, radio over fiber communication systems, and optical network security and management. He has published many high scientific research papers in high quality and technical international journals in the field of advanced communication systems, optoelectronic devices, and passive optical access communication networks. His areas of interest and experience in optical communication systems, advanced optical communication networks, wireless optical access networks, analog communication systems, optical filters and Sensors. As well as he is editorial board member in high academic scientific International research Journals. Moreover he is a reviewer member in high impact scientific research international journals in the field of electronics, electrical communication systems, optoelectronics, information technology and advanced optical communication systems and networks. His personal electronic mail ID (E-mail:ahmed\_733@yahoo.com). His published paper under the title "**High reliability optical interconnections for short range applications in high performance optical communication systems**" in *Optics and Laser Technology*, Elsevier Publisher has achieved most popular download articles in 2013.