

750kv Transmission Line parameter and line Efficiency calculation and the performance of High Voltage alternating current Transmission system using MATLAB program

Alka Szeerin Mansoori

M.E. Student of Electrical Engineering Department, Jabalpur Engineering College, Jabalpur
Under guidance of Associate Professor. Mrs. Ranjana Nigam Singh. Professor Electrical Engg. Department, Jabalpur Engineering College, Jabalpur

Abstract— This paper presents the electrical system for 750kv transmission line and also that have been built throughout the world to operate above 700kv. This paper provides information of system planning, design and programming of the transmission line. In this paper discussed by the overhead high voltage 3-phase transmission line problem. The problem is that: 750kv transmission line, its distance 500km, and its handling capacitive load is 2000MW calculate and discussed. These papers also consider that important that the design and operation of transmission line parameter and efficiency determination. The line losses and the efficiency of transmission depends on line parameter. These values are greatly influenced by the line constant R, L and C of transmission line. For instance of voltage drop in the line depends upon the above value of line parameter. The system performance is tested under steady-state condition. The line parameters and performance have been calculated by using several MATLAB functions, with MATLAB programs of transmission line analyzes the behavior and parameter of transmission line under the shunt compensation condition to a long transmission line and performance sending end and receiving end. The results after simulation help in designing of extra high voltage long transmission line model. This paper also shows that two conditions of transmission line: with and without shunt compensation. The intent of this paper is to provide information power handling capacity per circuit, number of circuits sag, average height, L, C, line parameter ABCD, receiving end current, sending end voltage, current, and power, line losses, and line efficiency.

Keywords: Overhead high voltage transmission line, Shunt compensation, MATLAB programming.

Introduction: Once high voltage AC power transmission became feasible in this century. The use of increasingly higher voltages for transmitting power efficiency over long distance. Higher voltage

transmission lines were also essential for the development of large interconnected power networks. This paper is considered that the capacity of transmission lines is becoming the main bottleneck of electricity transmission in the unregulated power industry [1]. The competition of electricity may aggravate the load ability of some transmission lines. To meet the load demands in a power system and to satisfy the stability and reliability criteria, the transmission lines must be utilized more efficiently. The purpose of the transmission network is to pool power plants and load centers in order to supply the load at a required reliability and maximum efficiency at a lower cost. A technically attractive solution to above problems is to use some efficient controls with the help of general MATLAB program. The transmission line parameters have been obtained and efficiency has been calculated on that transmission line. This paper also discussed with and without shunt compensation condition as the same high voltage transmission line problem at same distance and for same power frequency [2]. The results reveal that: Power transfer capability and voltage profile of transmission line is improved with compensating device. Moreover the software package developed using MATLAB is found to be quite useful as its working is independent of transmission line length and impedance of with and without shunt compensation device. The results demonstrate the performance of transmission line when the location of compensating device is varied [3].

Performance Analysis of Compensated Transmission Line

Consider that the transmission line parameters are uniformly distributed and the line can be modeled by a two-port, four-terminal network. Electrical power transmission lines have three main parameters, namely, resistance, inductance, and capacitance. These parameters are uniformly distributed along the entire length of the transmission lines. The inductive

reactance of a transmission line, which is directly proportional to the line inductance and the system frequency, is by far the most important line parameter because for normal line design, the power transfer capability is highly affected by its magnitude. Hence, the inductive reactance of transmission lines becomes a problem of increasing importance when transmission line length continues to increase [1, 2]. A decrease in the line inductive reactance increases the power transfer capability. Paralleling two or more similar lines is very effective in reducing the line inductive reactance since the inductive reactance decreases in inverse proportion to the number of lines. However, this method is not well practiced because of economic considerations [3, 4].

Shunt Controllers: The shunt controllers may be variable impedance, variable source, or a combination of these. In principle, all shunt Controllers inject current into the system at the point of connection. As long as the injected current is in phase quadrature with the line voltage, the shunt Controller only supplies or consumes variable reactive power. For handling real power other phase relationships are required. E.g. of shunt controllers[3,4]

Series Controllers: The series Controller could be variable impedance, such as capacitor, reactor, etc., or power electronics based variable source of main frequency, sub synchronous and harmonic frequencies to serve the desired need. In principle, all series controllers inject voltage in series with the line. As long as the voltage is in phase quadrature with the line current, the series controller only supplies or consumes variable reactive power. Any other phase relationship will involve handling of real power as well. e.g. of series controllers[3,4]

Design factor under steady state:

Design can be considered as synthesis of analytical procedures that are available and an enumerations of the limits and constraints under which line designs have to be carried out. The steady-state considerations are following:

1. Maximum allowable bus voltage and across equipment for a given voltage level.
2. Bundling, energy for these factor s are important for fixing the conductor diameter and number of conductors in the bundle and have been discussed.
3. Electrostatic field under the line at 50Hz covered.

4. Compensation requirements for voltage control as described.

MATLAB Module:-

An equations and constraints can be given here:

- a. Number of circuit:

The power handling capacity of single circuit

$$P=0.5V^2/(Lx) \text{ MW/circuit}$$

Where:

V =voltage in kV line-line;

L =line length in km;

x =total series reactance per km per phase.

r =line resistance per km per phase

$$\% \text{ power loss is } p=50 r/x;$$

- b. Line clearance and phase spacing:

NESC recommends a minimum clearance of 29 feet= 8.84meters for first 33kv and 0.52 meter extra for each 33kv.

$$\text{Average height } H = H_{\min} + S/3;$$

Where;

H_{min}=minimum clearance height,

S=sag

- c. Conductor Size and Number in bundle: Using formula;

For the centre phase E_{mc};

$$E_{mc} = V_m [1 + (N-1)r/R] / [Nr \ln \{ 2HS/req \sqrt{(4H^2 + S^2)} \}]$$

For the outer phases E_{mo};

$$E_{mo} = V_m / (Nr) [1 + (N-1)r/R] / [\ln(2H/req) - 0.5 \ln \{ \sqrt{(4H^2 + S^2)} (H^2 + S^2) / S^2 \}]$$

Where;

V_m=maximum operating voltage,

N =number of conductors in the bundle,

R =bundle radius,

r =radius of each conductor,

B = bundle spacing,

$$R = B/2 \sin(\pi/N)$$

$$req = \sqrt[N]{rB}$$

- d. Electrostatic field:

The potential coefficient matrix elements;

$$P_{ii} = \ln(2H/req)$$

$$P_{oc} = \ln((2H/S)^2 + 1)$$

$$P_{oo} = \ln((H/S)^2 + 1)$$

e. Line compensation Requirements:

From the [P] matrices, the average values of positive-sequence inductance and capacitance are calculated:

$$L_s = 0.2 \sum_{i=1}^3 P_{ii} \text{ mH/km}$$

$$L_m = 0.2(2P_{oc} + P_{oo}) \text{ mH/km}$$

$$L_+ = L_s - L_m; \text{ mH/km}$$

$$X_+ = 2\pi f L_+ \text{ ohm/km}$$

$$C_s = 2\pi\epsilon_0 \sum_{i=1}^3 M_{ii} \text{ nF/km}$$

$$C_m = 2\pi\epsilon_0 (2M_{oc} + M_{oo}) \text{ nF/km}$$

So, $C_+ = C_s - C_m; \text{ nF/km}$

$$y = 2\pi f C_+ \text{ mho/km}$$

Line Impedance: $Z = (R + jX_+) L$

Line Admittance: $Y = jyL$

Surge Impedance: $Z_0 = \sqrt{(Z/Y)}$

Voltage Control at power frequency:

- I. For line only: line parameter ABCD formula is mentioned below-

$$A = \cosh(\sqrt{ZY})$$

$$B = Z_0 \sinh(\sqrt{ZY})$$

$$C = \sinh(\sqrt{ZY})/Z_0$$

$$D = A;$$

Receiving - End Power –Circle:-

Centre of x-axis and y-axis:

$$x_c = -|V^2 A/B| \cos(\theta_a - \theta_b)$$

$$y_c = -|V^2 A/B| \sin(\theta_a - \theta_b)$$

$$\text{Radius} = |E_r E_s / B|$$

Where $E_r = V$; Receiving end voltage,

The compensation required is:-

$$(\text{Radius})^2 = (P/n + |x_c|)^2 + (|y_c| - Qr)^2$$

Where, n = no. of per circuit

The sending end voltage and current are calculated. The load at the receiving end is:

$$W_r = P/n + jQr; \text{ MVA}$$

Receiving end current is:-

$$I_r = W_r / \sqrt{3} \text{ V; k Amp per phase}$$

Equations for (E_s , I_s) in term of (E_r , I_r) are given below:-

$$\begin{bmatrix} E_s \\ I_s \end{bmatrix} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} \begin{bmatrix} E_r / \sqrt{3} \\ I_r \end{bmatrix}$$

The Sending – End Power is:-

$$W_s = \sqrt{3} E_s I_s; \text{ MVA}$$

Therefore the line loss is:-

$$P_l = \text{Re}(W_s) - P/n; \text{ MW, 3-phase}$$

The % line loss is = $100 P_l / \text{Re}(W_s)$

And the efficiency of transmission line is:-

$$\text{Eff} = 100 (P/n) / \text{Re}(W_s)$$

II. Shunt Reactor Compensation:-

The shunt compensate line parameter A_t , B_t , C_t , D_t calculate with the help of line parameter ABCD and use analytical equation shown below and

also show that Relation equation shunt compensate line parameter sending end voltage and current in term of receiving end voltage and current. Same procedures for calculation line loss and transmission line efficiency with shunt compensate.

$$\begin{bmatrix} At & Bt \\ Ct & Dt \end{bmatrix} = \begin{bmatrix} A & B \\ C & D \end{bmatrix} - jBl \begin{bmatrix} B & 0 \\ 2A - jBl & B \end{bmatrix}$$

Where,

Reactor admittance = $B_l = 1/X_{sh}$;

When a shunt compensating device is placed at a distance of x km from the sending end, the resultant generalized circuit constants of the compensated transmission line, with reactance X_{sh} of the shunt element respectively.

The value of compensating device depends up on the following constraints such as :

• Market Availability:

By compensation studies, if one needs a value of capacitor for a specific transmission line for a how much degree of compensation, that value may not be available in the market. Hence, whatever value is available; one has to make use of that. In that case, the degree of compensation would be different from the determined value.

• Available Location for the Capacitor Placement:

By compensation method, one might have arrived at an optimum location for the placement of the compensation scheme. At that location, there might not be a sub-station to place the compensation method. If so, then formation of a new sub-station exclusively for this purpose becomes an expensive affair. Instead, if there does a sub-station exist closer to the study-based optimum location, then that existing sub-station would be preferred for locating the compensation scheme. For such a situation, the degree of compensation as decided might be some different [3].

• Expected Increase in Power Transfer:

Before deciding the degree of compensation, all the parameters should be considered to ascertain whether the existing line can cope with the increased amount of power because of compensation.

• Transmission Efficiency:

With increased compensation at heavier loadings, the transmission losses increase steeply. The transmission efficiency is low. The compensation corresponding to maximum received power cannot be adopted. Hence, to improve efficiency of power transmission, though series compensation is considered, a small amount of shunt reactive volt-ampere is required at the receiving end. The power handling capacity can be increased; series capacitor compensation results in certain harmful properties in the system like increased short-circuit current and sub-harmonic or sub-synchronous resonance conditions during load changes and short circuits[3,4,5].

Case Study

The following transmission line parameters are obtained from HVAC transmission system. These data described below table are obtained by using MATLAB program for with and without shunt compensation. The following results are obtained:

Transmitted to the power in receiving end in MW
 $P_l = 2000$

Voltage in KV $V = 750$

Line length in Km $= 500$

Total series reactance per Km per phase $X = .272$

Minimum Clearance height in Meter $H_{min} = 13$

The max Operating voltage in KV $V_{max} = 765/\sqrt{3}$

The No. of conductor in the bundle $N = 4$

The bundle spacing in Meter $B_s = .4572$

Bundle sub-conductor radius in Meter $r = .015$

Distance from the outer phase at the ground in meter
 $D_o = 15$

The line resistance per Km per phase $R_l = .0136$

The value of shunt reactor admittance $= 1.037 * 10^{-3}$

Frequency in Hz $= 50$

Table: Output Result for line parameter of above input data based on MATLAB program performance:-

S. No.	Provide output	Line parameter without compensation	With Shunt compensation
1	power handling capacity in MW per ckt P	2068.01	2068.01
2	No. of ckt n	1	1
3	Horizontal span in Meter (Sag) S	15.14	15.14
4	Average height in Km Hav	18.0477	18.0477
5	bundle Radius in Meter R	0.161645	0.161645
6	Eq. radius in Meter Req	0.082813	0.082813
7	Mid Center Voltage in KV/m Emc	1838.45	1838.45
8	Mid Outer Voltage in KV/m Emo	1754.1	1754.1
9	Corona Inception Gradient Voltage Eor	1999.45	1999.45
10	Percentage of center phase margin PHm	8.05227	8.05227
11	percentage of outer phase margin OPm	12.2712	12.2712
12	The Average value of positive-sequence inductance Lp	0.972352	0.972352
13	The Positive Inductance Xpositive	0.305474	0.305474
14	The Average value of positive-sequence capacitance Cp	11.4897	11.4897
15	y in mho/km	3.60959	3.60959
16	Total series impedance of line Z Real, imag, abs, angle	6.8, 152.737, 152.888, 87.4508	6.8, 152.737, 152.888, 87.4508
17	Total shunt admittance of line Y Real, imag, abs, angle	0, 0.00180479, 0.00180479, 90	0, 0.00180479, 0.00180479, 90
18	Surge impedance of Zo Real, imag, abs, angle	290.982, -6.4742, 291.054, -1.27459,	290.982, -6.4742, 291.054, -1.27459,
19	Line parameter Re, imag, abs, angle	A=0.865302,0.00585823, 0.865322,0.387896, B=6.18797,145.829, 145.96,87.5702, C=-3.59081e-6,0.00172301, 0.00172301,90.1194, D= A	At=1.01607,-0.000540886, 1.01607,-0.0305004, Bt=6.18795,145.392, 145.524,87.5629; Ct=1.91987e-006, -0.000222738, 0.000222746,-89.5062, Dt=At
20	The Receiving-End Wr Total Load	2002.84,	2076.28,
21	Receiving-End current in KA 3-phase in	1.56496	1.5396
22	Sending Voltage in Kv line to ground, line to line	454.856, 787.833	446.975, 774.184
23	Sending Current per phase in KAmP	1.59148	1.38669

24	Sending-end power MW	2443.97	2081.83
25	Percentage of power line loss	18.1658%	3.93047%
26	Efficiency of transmission line	81.8342%	96.0695%

These results are obtained by MATLAB program and shown above table. It is concluded that in the considered transmission line, if the available compensating device is 1.037×10^{-3} Ohms shunt reactor admittance. Than eff. Improve 14.8608%.

Conclusion

This paper focus on the parameter design of the transmission line system and it line efficiency. The results for the system are obtained by the MATLAB program and output result shown that above table. For compared and calculate the line parameter and efficiency of two conditions with and without shunt compensation of transmission line with admittance reactor Bl. Output result table clearly shown that the condition of with shunt compensation line efficiency improve that condition of without compensation line efficiency and it losses are reduced. Where it is placed. It is not necessary that a device which is transferring maximum power will also be minimizing the reactive losses.

The results found in this work would be very useful in selecting the best for shunt compensation show that table. It is also discussed that the shunt controllers, sag, average height, power handling capacity per circuit, center phase, outer phase, electrostatic field, average value of positive sequence inductance and capacitance, line impedance, admittance, surge impedance, line parameter and receiving end power also calculate the line efficiency and line losses with and without compensation of ac transmission systems, providing multifunctional flexibility required to solve many of the problems facing the power delivery industry. These controllers are able to control, simultaneously or selectively, all the parameters affecting power flow in the transmission line (i.e. voltage, impedance and phase angle).

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